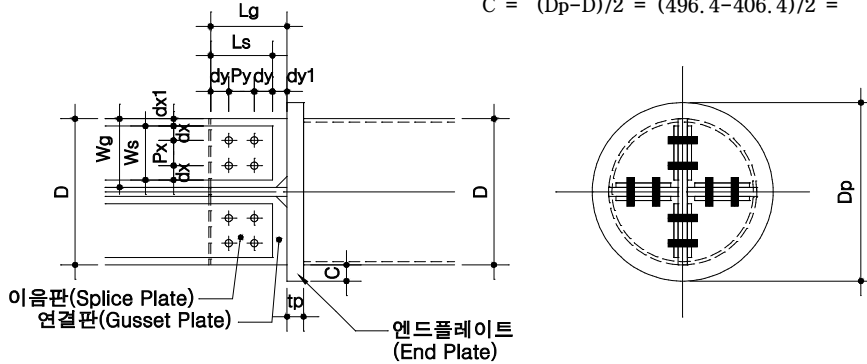


1. 설계조건

* 원형강관	Fy =	235 MPa	D =	φ406.4 mm	Ag =	11200 mm ²
	Fu =	400 MPa	t =	9 mm		
* 엔드플레이트	Fye =	355 MPa	Dp =	φ496.4 mm		
	Fue =	520 MPa	tp =	45 mm		
			C = (Dp-D)/2 =	(496.4-406.4)/2 =	45.0 mm	



2. 소요인장용량

$$\begin{aligned}\phi P_n &= \phi t F_y A_g = 0.9 \times 235 \times 11200 \times 1/10^3 = 2368.8 \text{ kN} \\ \phi P_n &= \phi t F_u A_e = \phi t F_u U A_n = 0.75 \times 400 \times 1 \times 11200 \times 1/10^3 = 3360.0 \text{ kN} \\ A_n &= A_g = 11200 \text{ mm}^2 \quad U = 1.00\end{aligned}$$

$$\therefore P_{u, req} = \text{MIN}(2368.8, 3360) = 2368.8 \text{ kN}$$

3. 연결판 및 이음판 검토

1) 고력볼트 / 마찰접합 검토

(1group당)									
고력볼트	직경 Db(mm)	구멍직경 Dbh(mm)	열수 Nx(열)	행수 Ny(행)	전체개수 N(EA)	볼트간격 Px(mm)	볼트간격 Py(mm)	연단거리 dx(mm) dx1(mm)	연단거리 dy(mm) dy1(mm)
F10T	M20	22	2	2	4	70	70	40 20.2	50 40

$$W_{g, req} \geq (N_x - 1) \cdot P_x + 2 \cdot dx + dx1 = (2 - 1) \cdot 70 + 2 \cdot 40 + 20.2 = 170.2 \text{ mm}$$

$$L_{g, req} \geq (N_y - 1) \cdot P_y + 2 \cdot dy + dy1 = (2 - 1) \cdot 70 + 2 \cdot 50 + 40 = 210.0 \text{ mm}$$

$$\phi = 1.00 \quad \mu = 0.50 \quad (\text{블라스트 후 페인트하지 않은 경우})$$

$$hf = 1.00 \quad F_u = 1000 \text{ MPa} \quad A_b = 314.2 \text{ mm}^2/\text{EA} \quad \text{전단면의 수 } N_s = 2$$

설계볼트장력

$$T_o = 0.70 \cdot F_u \cdot 0.75 \cdot A_b = 0.70 \cdot 1000 \cdot 0.75 \cdot 314.2 = 165.0 \text{ kN/EA}$$

$$\phi R_n = \phi \cdot \mu \cdot hf \cdot T_o \cdot N_s = 1 \cdot 0.5 \cdot 1 \cdot 165 \cdot 2 = 165.0 \text{ kN/EA}$$

$$\therefore P_{u, req} / \phi R_n = 2368.8 / 165 = 14.36 \text{ EA} \leq 16 \text{ EA} \quad \dots \text{OK}$$

2) 이음판(Splice Plate)

Fys =	235	MPa	매수	폭	길이	두께	면적	구멍개수	구멍직경	공제면적
Fus =	400	MPa		Ws (mm)	Ls (mm)	ts (mm)	(mm ²)		(mm)	(mm ²)
			2	150	170	12	3600	2	22	-1056
			Σ			24	3600			-1056

(1) 인장항복강도

$$A_g = 3600 \text{ mm}^2$$

$$\phi P_n = \phi t * F_y * A_g = 0.9 * 235 * 3600 * 1/10^3 * 4_{\text{group}} = 3045.6 \text{ kN}$$

$$\therefore P_u, \text{req}/\phi P_n = 2368.8 / 3045.6 = 0.78 \leq 1.00 \dots \text{OK}$$

(2) 인장파단강도 $U = 1.00$

$$A_n = \text{MIN}(3600 + (-1056), 0.85 * A_g) = \text{MIN}(2544, 0.85 * 3600) = 2544.0 \text{ mm}^2$$

$$\phi P_n = \phi t * F_u * A_e = \phi t * F_u * U * A_n = 0.75 * 400 * 1 * 2544 * 1/10^3 * 4_{\text{group}} = 3052.8 \text{ kN}$$

$$\therefore P_u, \text{req}/\phi P_n = 2368.8 / 3052.8 = 0.78 \leq 1.00 \dots \text{OK}$$

(3) 블록전단강도

$$L = (N_y - 1) * P_y = (2 - 1) * 70 = 70.0 \text{ mm}$$

* 인장저항 순단면적

$$A_{nt} = A_{gt} - D_{bh} * (N_x - 0.5) * t_s = 2640 - 22 * (2 - 0.5) * 24 = 1848.0 \text{ mm}^2$$

* 인장저항 총단면적

$$A_{gt} = (P_x + d_x) * t_s = (70 + 40) * 24 = 2640.0 \text{ mm}^2$$

* 전단저항 순단면적

$$A_{nv} = A_{gv} - D_{bh} * (N_y - 0.5) * t_s = 2880 - 22 * (2 - 0.5) * 24 = 2088.0 \text{ mm}^2$$

* 전단저항 총단면적

$$A_{gv} = (L + d_y) * t_s = (70 + 50) * 24 = 2880.0 \text{ mm}^2$$

$$F_u * A_{nt} = 400 * 1848 * 1/10^3 = 739.2 \text{ kN}$$

$$0.6 * F_u * A_{nv} = 0.6 * 400 * 2088 * 1/10^3 = 501.1 \text{ kN}$$

$$F_y * A_{gt} = 235 * 2640 * 1/10^3 = 620.4 \text{ kN}$$

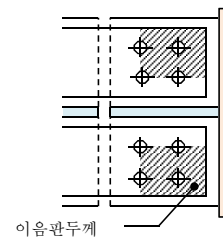
$$0.6 * F_y * A_{gv} = 0.6 * 235 * 2880 * 1/10^3 = 406.1 \text{ kN}$$

$$U_{bs} = 1.00$$

$$\phi P_n = \phi t * (U_{bs} * F_u * A_{nt} + \text{MIN}(0.6 * F_u * A_{nv}, 0.6 * F_y * A_{gv}))$$

$$= 0.75 * (1 * 739.2 + \text{MIN}(501.1, 406.1)) * 4_{\text{group}} = 3435.9 \text{ kN}$$

$$\therefore P_u, \text{req}/\phi P_n = 2368.8 / 3435.9 = 0.69 \leq 1.00 \dots \text{OK}$$



3) 연결판(Gusset Plate)

(1group당)

$F_{yg} = 355$ MPa	매수	폭	길이	두께	면적	구멍개수	구멍직경	공제면적
$F_{ug} = 520$ MPa		W_g (mm)	L_g (mm)	t_g (mm)	(mm^2)		(mm)	(mm^2)
Scallop, $Sc = 30$ mm	1	190.7	210	25	4767.5	2	22	-1100
	Σ			25	4767.5			-1100

$$\text{폭두께비 } b/t = W_g/T_g = 190.7/25 = 7.63 < 15.00 \dots \text{OK}$$

(1) 인장항복강도

$$A_g = 4767.5 * 4_{\text{group}} + 25 * 25 (\text{교차부}) = 19695.0 \text{ mm}^2$$

$$\phi P_n = \phi t * F_y * A_g = 0.9 * 355 * 19695 * 1/10^3 = 6292.6 \text{ kN}$$

$$\therefore P_u, \text{req}/\phi P_n = 2368.8 / 6292.6 = 0.38 \leq 1.00 \dots \text{OK}$$

(2) 인장파단강도 $U = 1.00$

$$A_n = \text{MIN}(19695 + (-1100 * 4_{\text{group}}), 0.85 * A_g) = \text{MIN}(15295, 0.85 * 19695) = 15295.0 \text{ mm}^2$$

$$\phi P_n = \phi t * F_u * A_e = \phi t * F_u * U * A_n = 0.75 * 520 * 1 * 15295 * 1/10^3 = 5965.1 \text{ kN}$$

$$\therefore P_u, \text{req}/\phi P_n = 2368.8 / 5965.1 = 0.40 \leq 1.00 \dots \text{OK}$$

(3) 블록전단강도

$$L = (N_y - 1) \cdot P_y = (2 - 1) \cdot 70 = 70.0 \text{ mm}$$

* 인장저항 순단면적

$$A_{nt} = A_{gt} - D_{bh} \cdot (N_x - 0.5) \cdot t_g = 3255 - 22 \cdot (2 - 0.5) \cdot 25 = 2430.0 \text{ mm}^2$$

* 인장저항 총단면적

$$A_{gt} = (P_x + d_x + d_{x1}) \cdot t_g = (70 + 40 + 20.2) \cdot 25 = 3255.0 \text{ mm}^2$$

* 전단저항 순단면적

$$A_{nv} = A_{gv} - D_{bh} \cdot (N_y - 0.5) \cdot t_g = 3000 - 22 \cdot (2 - 0.5) \cdot 25 = 2175.0 \text{ mm}^2$$

* 전단저항 총단면적

$$A_{gv} = (L + d_y) \cdot t_g = (70 + 50) \cdot 25 = 3000.0 \text{ mm}^2$$

$$F_{ug} \cdot A_{nt} = 520 \cdot 2430 \cdot 1/10^3 = 1263.6 \text{ kN}$$

$$0.6 \cdot F_{ug} \cdot A_{nv} = 0.6 \cdot 520 \cdot 2175 \cdot 1/10^3 = 678.6 \text{ kN}$$

$$F_{yg} \cdot A_{gt} = 355 \cdot 3255 \cdot 1/10^3 = 1155.5 \text{ kN}$$

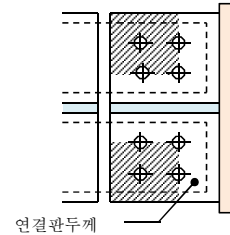
$$0.6 \cdot F_{yg} \cdot A_{gv} = 0.6 \cdot 355 \cdot 3000 \cdot 1/10^3 = 639.0 \text{ kN}$$

$$U_{bs} = 1.00$$

$$\phi P_n = \phi t \cdot (U_{bs} \cdot F_{ug} \cdot A_{nt} + \min(0.6 \cdot F_{ug} \cdot A_{nv}, 0.6 \cdot F_{yg} \cdot A_{gv}))$$

$$= 0.75 \cdot (1 \cdot 1263.6 + \min(678.6, 639.0)) \cdot 4_{\text{group}} = 5707.8 \text{ kN}$$

$$\therefore P_u, \text{req} / \phi P_n = 2368.8 / 5707.8 = 0.42 \leq 1.00 \dots \text{OK}$$



4) 연결판과 엔드플레이트 용접부

$$V_u = P_u, \text{req} / 4 = 2368.8 / 4 = 592.2 \text{ kN}$$

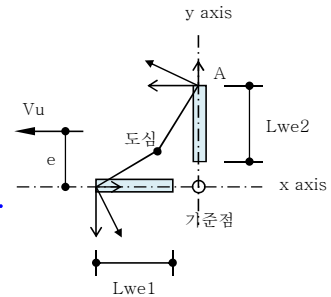
$$e = W_g / 2 + t_g / 2 = 190.7 / 2 + 25 / 2 = 107.9 \text{ mm}$$

$$M_u = V_u \cdot e = 592.2 \cdot 107.9 \cdot 1/10^3 = 63.90 \text{ kN-m}$$

용접치수 Sw1 = 25 mm (완전용입용접) 엔드탭 유무 : 없음.

$$L_{we1} = L_g - S_c - 2 \cdot S_{w1} = 210 - 30 - 2 \cdot 25 = 130.0 \text{ mm}$$

$$L_{we2} = W_g - S_c - 2 \cdot S_{w1} = 190.7 - 30 - 2 \cdot 25 = 110.7 \text{ mm}$$



가로치수 (mm)	세로치수 (mm)	면적 (mm ²)	도심거리 (mm)	면적*도심거리 (mm ³)	D (mm)	Ixo (mm ⁴)	A*D ² (mm ⁴)
1.0	110.7	110.7	110.4	12221.3	-59.63	113047.7	393620.1
130.0	1.0	130.0	0.0	0.0	50.77	10.8	335087.1
							0.0
Σ		240.7		12221.3		113058.5	728707.2

$$y_1 = \Sigma(\text{면적} \cdot \text{도심거리}) / \Sigma(\text{면적}) = 12221.3 / 240.7 = 50.77 \text{ mm}$$

$$y_2 = W_g - S_{w1} - y_1 = 190.7 - 25 - 50.77 = 114.93 \text{ mm}$$

$$I_x = 1 \cdot (\Sigma(I_{xo}) + \Sigma(A \cdot D^2)) = 1 \cdot (113058.5 + 728707.2) = 841766 \text{ mm}^4$$

가로치수 (mm)	세로치수 (mm)	면적 (mm ²)	도심거리 (mm)	면적*도심거리 (mm ³)	D (mm)	Iyo (mm ⁴)	A*D ² (mm ⁴)
110.7	1.0	110.7	0.0	0.0	64.81	9.2	464977.2
1.0	130.0	130.0	120.0	15600.0	-55.19	183083.3	395971.7
							0.0
Σ		240.7		15600.0		183092.5	860948.9

$$x_1 = \Sigma(\text{면적} \cdot \text{도심거리}) / \Sigma(\text{면적}) = 15600 / 240.7 = 64.81 \text{ mm}$$

$$x_2 = L_g - S_{w1} - x_1 = 210 - 25 - 64.81 = 120.19 \text{ mm}$$

$$I_y = 1 \cdot (\Sigma(I_{yo}) + \Sigma(A \cdot D^2)) = 1 \cdot (183092.5 + 860948.9) = 1044041 \text{ mm}^4$$

$$I_p = (I_x + I_y) \cdot S_{w1} = (841766 + 1044041) \cdot 25 = 47145175 \text{ mm}^4$$

* A점에서의 응력

$$dx = x1 = 64.81 \text{ mm} \quad dy = y2 = 114.93 \text{ mm}$$

$$\begin{aligned} ft &= Vu/A = 592.2 \times 10^3 / (25 \times 240.7) = 98.41 \text{ N/mm}^2 \\ fbt &= Mu \cdot dy / Ip = 63.9 \times 10^6 \times 114.93 / 47145175 = 155.77 \text{ N/mm}^2 \\ fbv &= Mu \cdot dx / Ip = 63.9 \times 10^6 \times 64.81 / 47145175 = 87.84 \text{ N/mm}^2 \\ fr &= \sqrt{(2.25 \cdot fbv^2 + (fbt + ft)^2)} = \sqrt{(2.25 \times 87.84^2 + (155.77 + 98.41)^2)} = 286.30 \text{ N/mm}^2 \end{aligned}$$

$$\begin{aligned} \phi_{rnw} &= \phi \cdot F_{yg} = 0.9 \times 355 = 319.50 \text{ N/mm}^2 \\ \therefore fr / \phi_{rnw} &= 286.3 / 319.5 = 0.90 \leq 1.00 \quad \dots \text{OK} \end{aligned}$$

4. 엔드플레이트 소요두께 산정

$$\begin{aligned} wut &= Pu, req / (\pi \cdot D^2 / 4) = 2368.8 \times 10^3 / (\pi \times 406.4^2 / 4) = 18.26 \text{ N/mm}^2 \\ * \text{단순지지판에서 방사선 방향의 최대 휨모멘트} \quad a &= D - 2 \cdot t = 406.4 - 2 \times 9 = 388.4 \text{ mm} \\ Mu, max &= 0.051 \cdot wut \cdot a^2 = 0.051 \times 18.26 \times 388.4^2 = 140485 \text{ N-mm/mm} \end{aligned}$$

$$\begin{aligned} \phi Mn &= \phi \cdot F_{ye} \cdot Z_x = 0.90 \times 355 \times (1 \times tp^2 / 4) = 79.88 \cdot tp^2 \text{ N-mm/mm} \\ \therefore tp, req &= \sqrt{(140485 / 79.88)} = 41.94 \text{ mm} \leq tp = 45 \text{ mm} \quad \dots \text{OK} \end{aligned}$$

* 완전용입용접인 경우 여장

$$C, req = t/4 + tp, req = 9/4 + 41.94 = 44.19 \text{ mm} \leq C = 45 \text{ mm} \quad \dots \text{OK}$$

5. 엔드플레이트와 원형강관 용접부 검토

$$\text{용접재 인장강도} \quad F_{uw} = 420 \text{ MPa}$$

- 용접치수

$$Sw2 = 9.00 \text{ mm} \quad nw = 1 \text{ 개소} \quad \text{필릿용접(1)/완전용입용접(2)} : 2$$

$$\begin{aligned} Lwe &= 2 \cdot \pi \cdot (D/2 - Sw2/2) = 2 \cdot \pi \cdot (406.4/2 - 9/2) = 1248.5 \text{ mm} \\ Aw &= nw \cdot Sw2 \cdot Lwe = 1 \times 9 \times 1248.5 = 11236.5 \text{ mm}^2 \end{aligned}$$

$$\begin{aligned} \phi Rn &= \phi \cdot F_u \cdot t \cdot Lwe = 0.75 \times 400 \times 9 \times 1248.5 \times 1/10^3 = 3371.0 \text{ kN} \\ \therefore Pu, req / \phi Rn &= 2368.8 / 3371 = 0.70 \leq 1.00 \quad \dots \text{OK} \end{aligned}$$

$$\begin{aligned} \phi Rn &= \phi \cdot F_y \cdot t \cdot Lwe = 0.9 \times 235 \times 9 \times 1248.5 \times 1/10^3 = 2376.5 \text{ kN} \\ \therefore Pu, req / \phi Rn &= 2368.8 / 2376.5 = 1.00 \leq 1.00 \quad \dots \text{OK} \end{aligned}$$